### Topographic beta-plane turbulence and form stress



Navid Constantinou & Bill Young Scripps Institution of Oceanography UC San Diego



thanks to IPAM

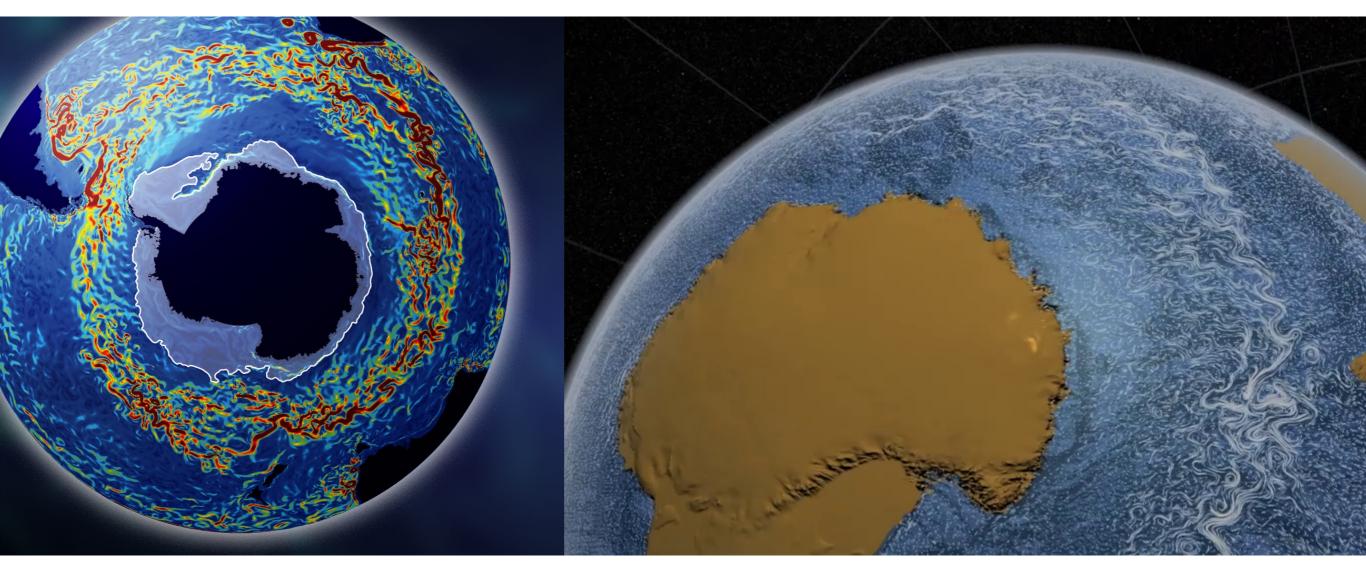
(work in progress)

7 June 2016

how does the bottom topography of the ocean affect the large-scale zonal oceanic currents?

(e.g. the Antarctic Circumpolar Current)

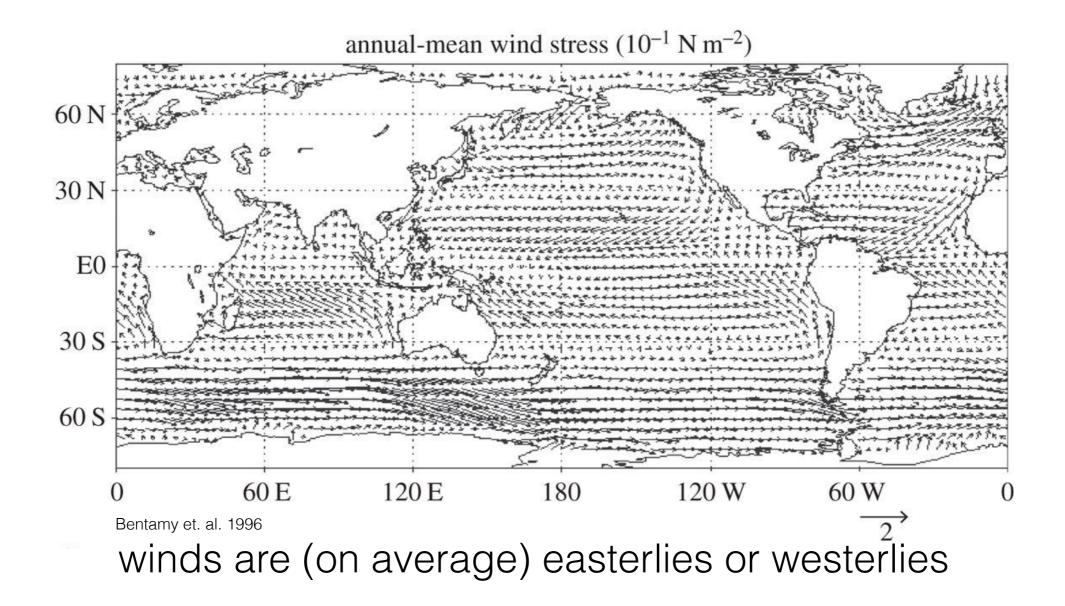
#### Antarctic Circumpolar Current (ACC)



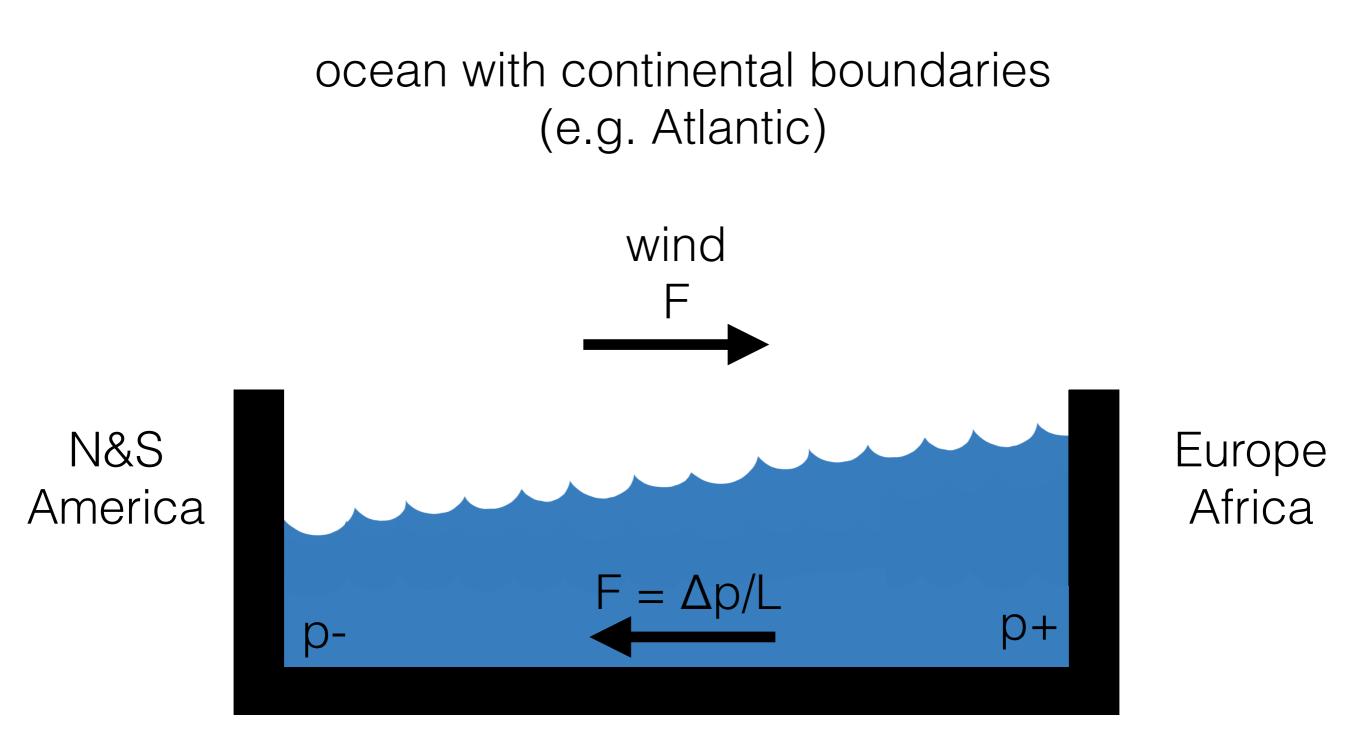
Southern Ocean State Estimate UC San Diego NASA/Goddard Space Flight Center

state estimates (computer simulations constrained by observations)

#### momentum is imparted to the ocean by winds

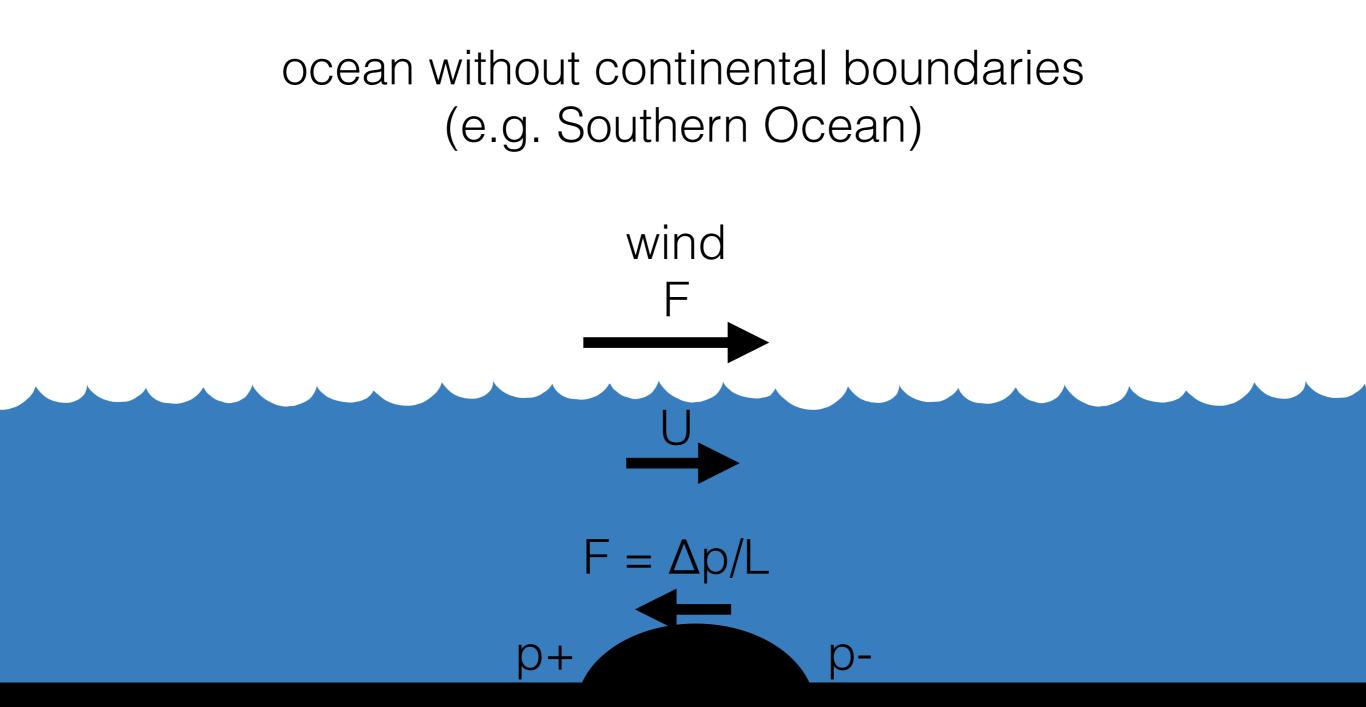


how does the force applied to the oceans by the winds balance?



the surface of the ocean tilts and creates an east-west pressure gradients that mostly balances the momentum input

(the ocean leans onto the eastern coast)



the flow over ocean ridges creates pressure differences that counterbalance the momentum input

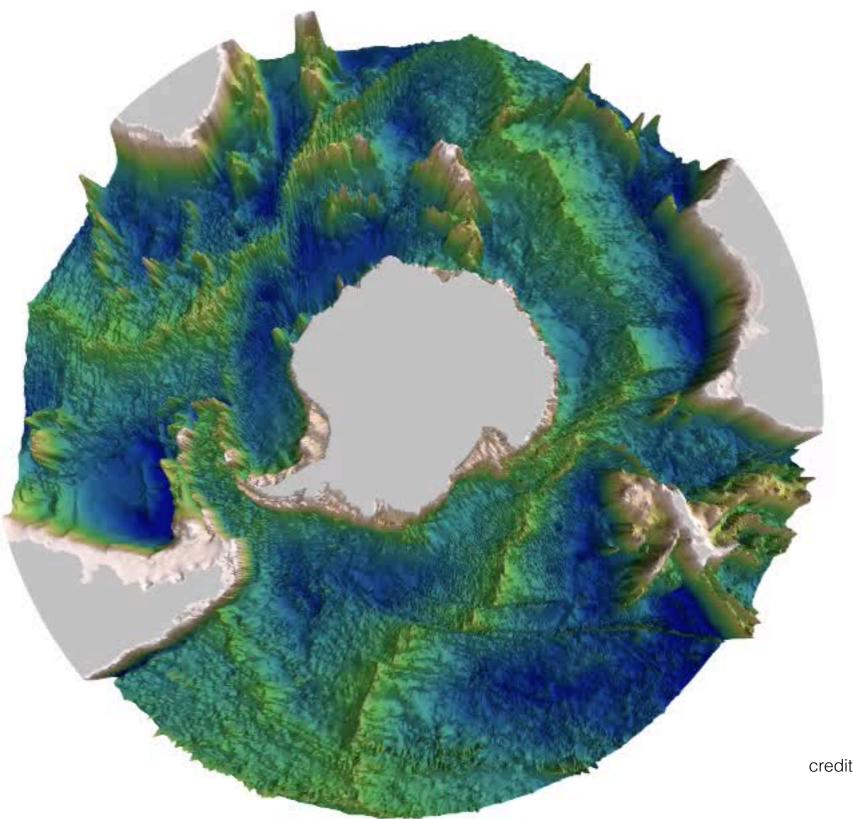


"I don't know why I don't care about the bottom of the ocean, but I don't." initially work didn't focus on the role of the bottom topography

in a seminal paper Munk & Palmen 1951 with a back-of-the-envelope calculation estimated that:

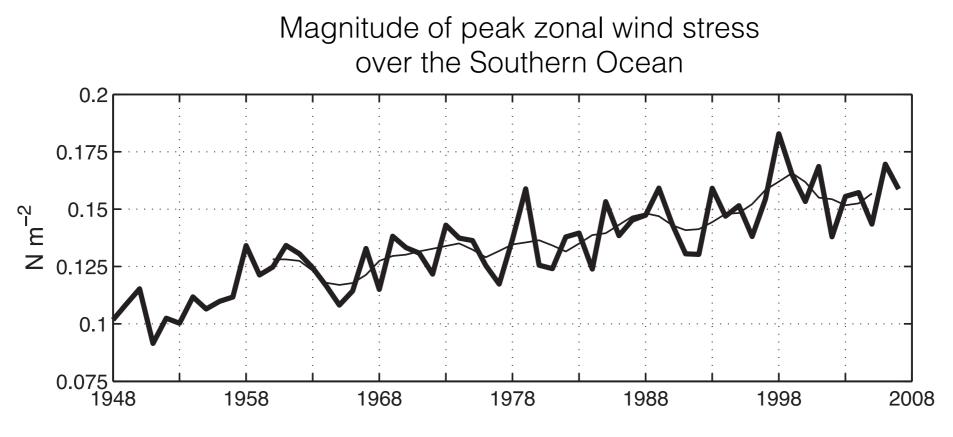
if the bottom of the Southern Ocean was flat then the ACC should be 10-20 times stronger than observed!

#### topography in the Southern Ocean



credit: V. Tamsitt, Scripps, UCSD

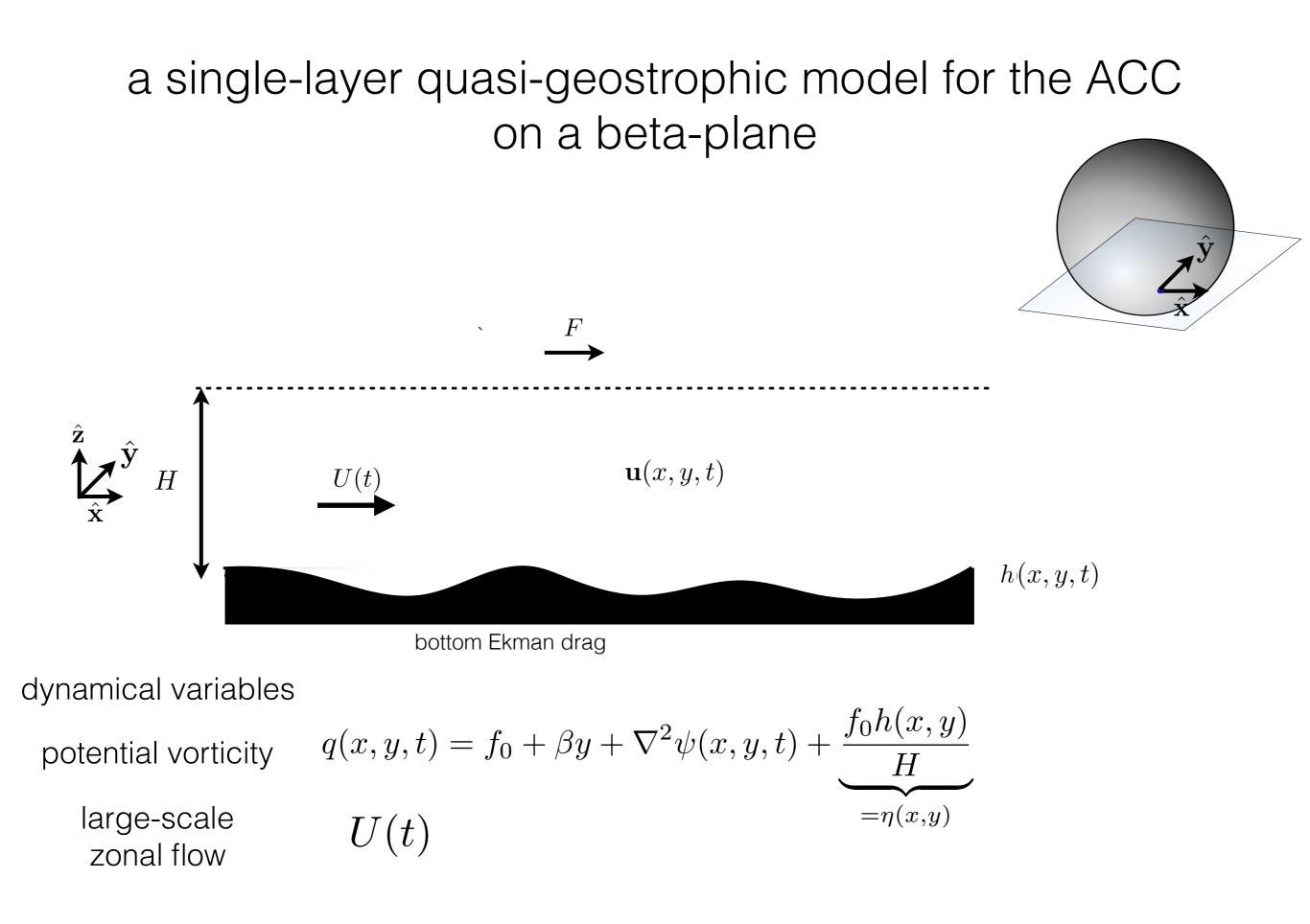
#### yet some more motivation...



Farneti et. al. 2015

winds seem to be increasing how will the ACC respond?

doubling the wind gives double the ACC? not always — "eddy saturation" regime



#### flow evolution

$$\partial_t q + \mathsf{J}(\psi - Uy, q) = -\mu \nabla^2 \psi$$
$$\partial_t U = F - \mu U - \langle \psi \partial_x \eta \rangle$$
$$q = f_0 + \beta y + \nabla^2 \psi + \eta$$

Hart 1979 Carnevale & Frederiksen 1989 Holloway 1989

where 
$$J(a,b) = (\partial_x a)(\partial_y b) - (\partial_y a)(\partial_x b)$$

=advection of *b* by the flow with stream function *a* 

$$\langle \bullet \rangle = \frac{1}{L^2} \int \bullet \mathrm{d}^2 \mathbf{x}$$

periodic boundary conditions in *x*,*y* 

domain = square of length L

#### parameters

$$\partial_t q + \mathsf{J}(\psi - Uy, q) = -\mu \nabla^2 \psi$$
$$\partial_t U = F - \mu U - \langle \psi \partial_x \eta \rangle$$
$$q = f_0 + \beta y + \nabla^2 \psi + \eta$$

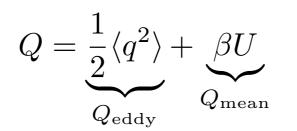
- F : mean wind stress
- $\beta$  : planetary vorticity gradient,  $\beta = df/dy$
- $\mu$  : bottom Ekman drag coefficient

$$\eta(\mathbf{x})$$
 : topography  $\eta_{\rm rms} = \sqrt{\langle \eta^2 \rangle}$   
 $\ell_{\eta} = \sqrt{\eta_{\rm rms}^2 / \langle |\nabla \eta|^2 \rangle}$   
spectral distribution (e.g. isotropic)  
spectral slope (for isotropic)

#### energy & potential enstrophy

$$\partial_t q + \mathsf{J}(\psi - Uy, q) = -\mu \nabla^2 \psi$$
$$\partial_t U = F - \mu U - \langle \psi \partial_x \eta \rangle$$
$$q = f_0 + \beta y + \nabla^2 \psi + \eta$$

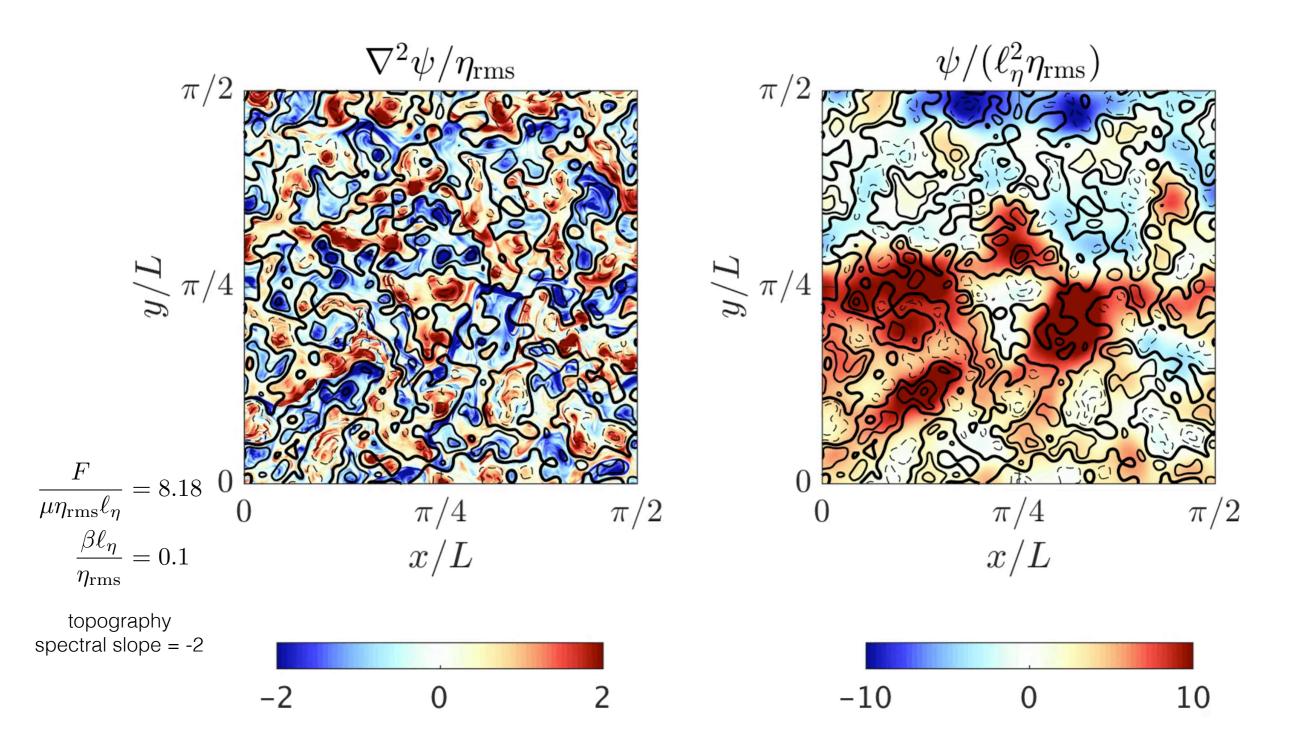
$E = \frac{1}{2} \langle  \nabla \psi ^2 \rangle +$	$-\frac{1}{2}U^2$
$E_{ m eddy}$	$E_{\mathrm{mean}}$



$$\frac{\mathrm{d}E}{\mathrm{d}t} = FU - \mu U^2 - \mu \langle |\nabla \psi|^2 \rangle$$
$$\frac{\mathrm{d}Q}{\mathrm{d}t} = F\beta - \mu\beta U - \mu \langle (\nabla^2 \psi + \eta) \nabla^2 \psi$$

total energy and potential enstrophy are conserved in the absence of forcing and dissipation

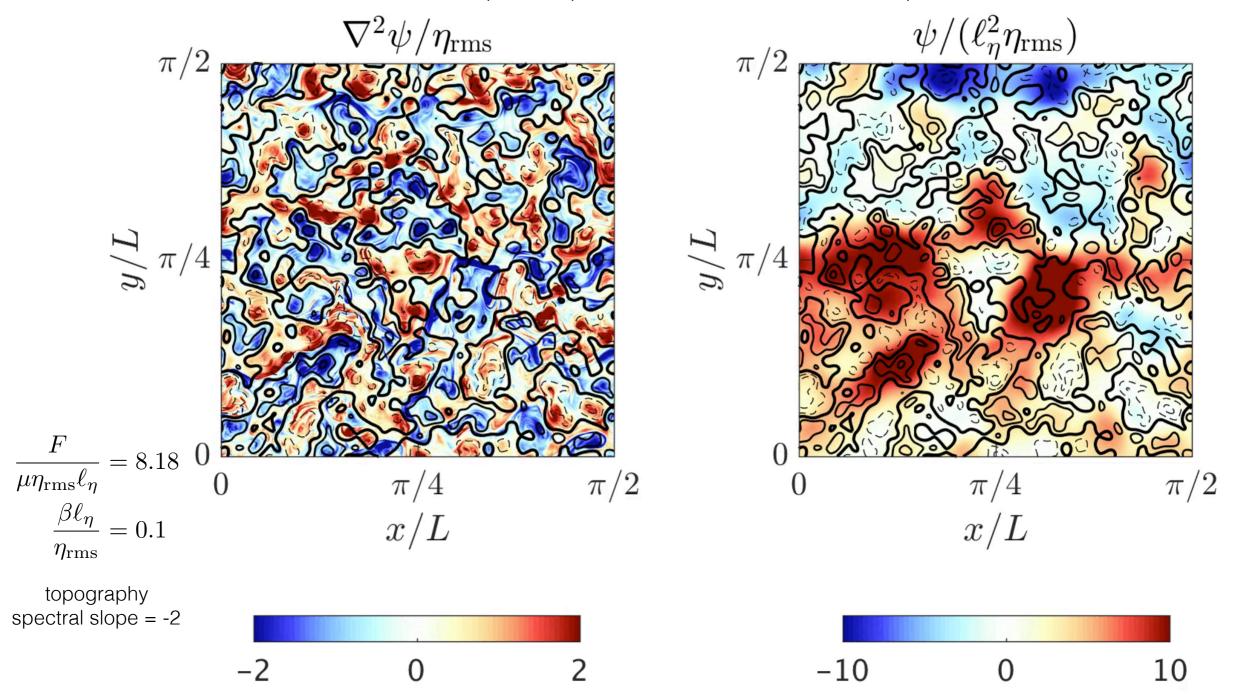
# a snapshot of the flow at statistically steady state for "realistic" parameter values $\mu t = 4.00$



#### spin-up from rest

 $\mu t = 4.00$ 

http://www-pord.ucsd.edu/~navid/animation.mp4



topographic form stress

$$\partial_t U = F - \mu U - \langle \psi \partial_x \eta \rangle$$
topographic form stress
(or pressure drag)
(or mountain drag)
(or form drag)

form stress controls the steady state large-scale U

for a flat bottom 
$$\overline{U} = \frac{F}{\mu}$$
 very large  
(Munk & Palmen 1951)  
for a non-flat bottom  $\overline{U} = \frac{F - \overline{\langle \psi \partial_x \eta \rangle}}{\mu}$ 

#### a bound for the form stress based on the energy equation

$$\mathcal{F}\left[\psi\right] = \overline{\langle\psi\partial_x\eta\rangle} + \lambda_1 \left(F - \mu\overline{U} - \overline{\langle\psi\partial_x\eta\rangle}\right) + \lambda_2 \left(F\overline{U} - \mu\overline{U}^2 - \overline{\langle\mu|\nabla\psi|^2\rangle}\right)$$

$$\overset{\mathbf{k}}{\underset{\text{mean flow}}{\text{steady state}}} \qquad \overset{\mathbf{k}}{\underset{\text{energy}}{\text{equation}}}$$

$$\overline{\langle\psi\partial_x\eta\rangle} \leq \frac{F}{1 + \frac{\mu^2}{\gamma[\eta]}} \qquad \gamma[\eta] = \sum_{\mathbf{k}} \frac{k_x^2}{|\mathbf{k}|^2} |\hat{\eta}(\mathbf{k})|^2$$

a bound for the form stress based on the energy equation + the enstrophy equation

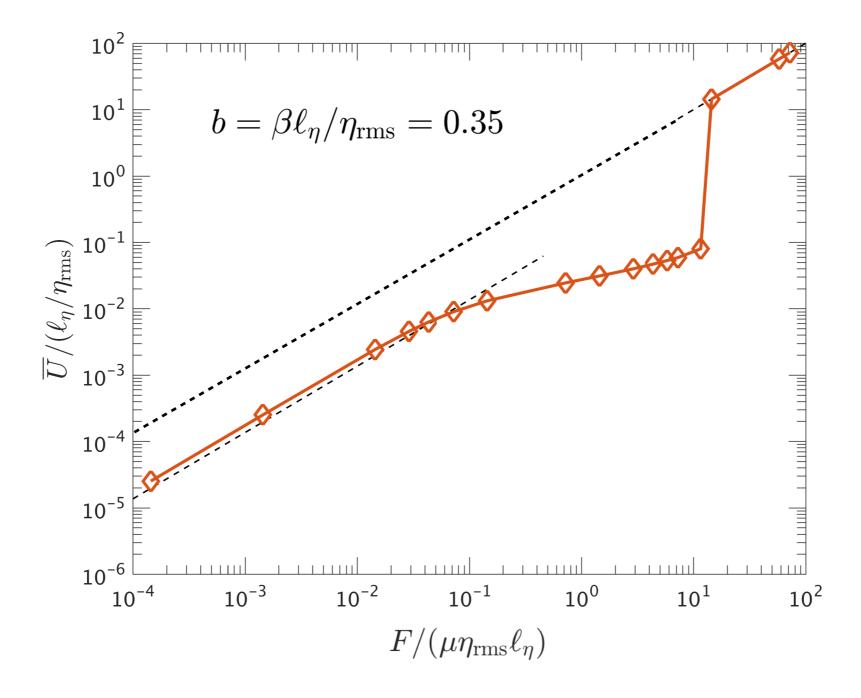
$$\mathcal{F}[\psi] = \overline{\langle \psi \partial_x \eta \rangle} + \lambda_1 \left( F - \mu \overline{U} - \overline{\langle \psi \partial_x \eta \rangle} \right) + \lambda_2 \left( F \overline{U} - \mu \overline{U}^2 - \overline{\langle \mu | \nabla \psi |^2 \rangle} \right) + \lambda_3 \left( F \beta - \mu \beta \overline{U} - \mu \overline{\langle (\nabla^2 \psi + \eta) \nabla^2 \psi \rangle} \right)$$

steady state enstrophy equation

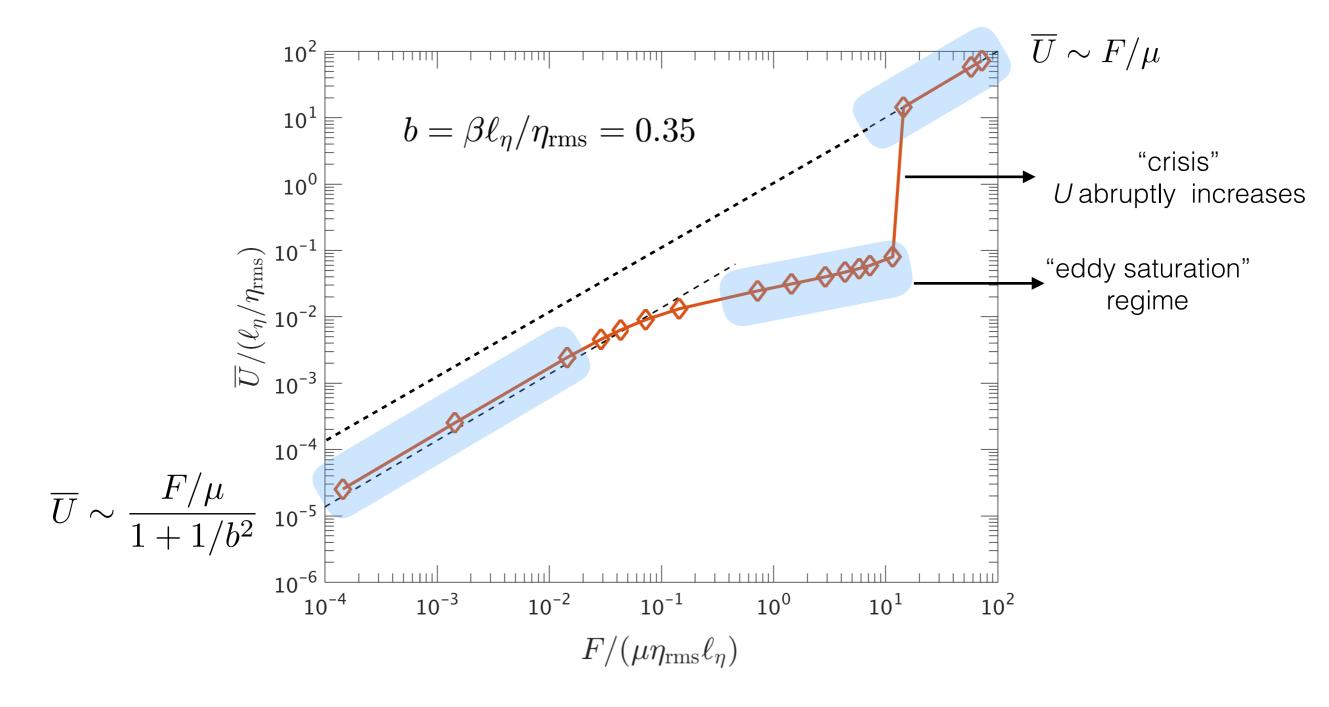
we were unable to obtain a bound...

are we over restricting the problem?

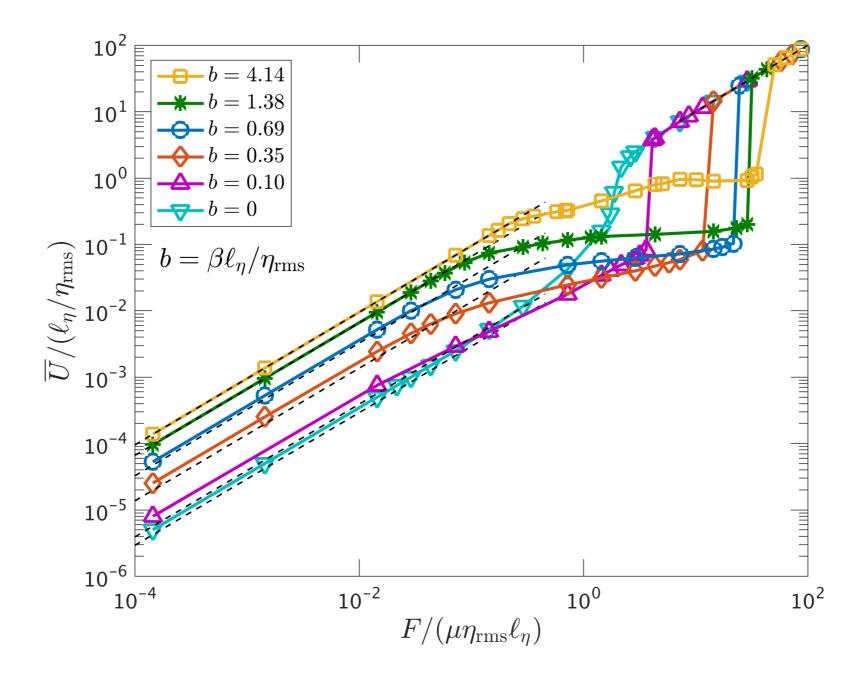
any suggestions perhaps?



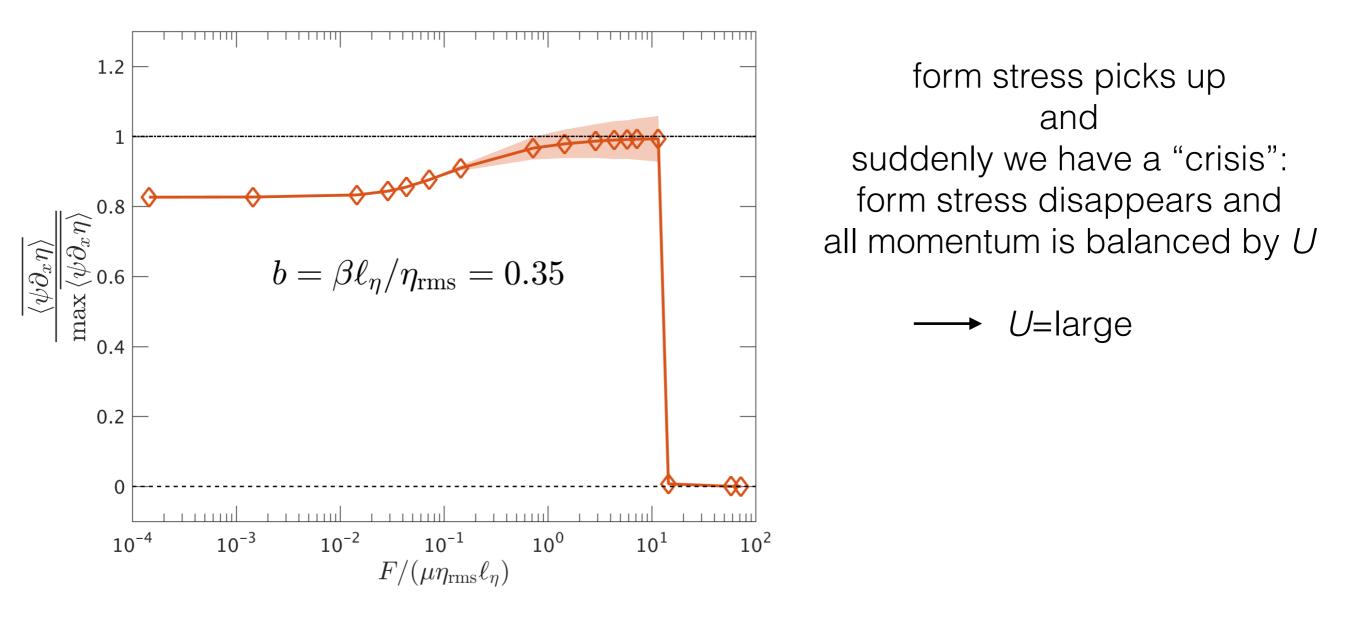
#### how does U respond to wind increase?



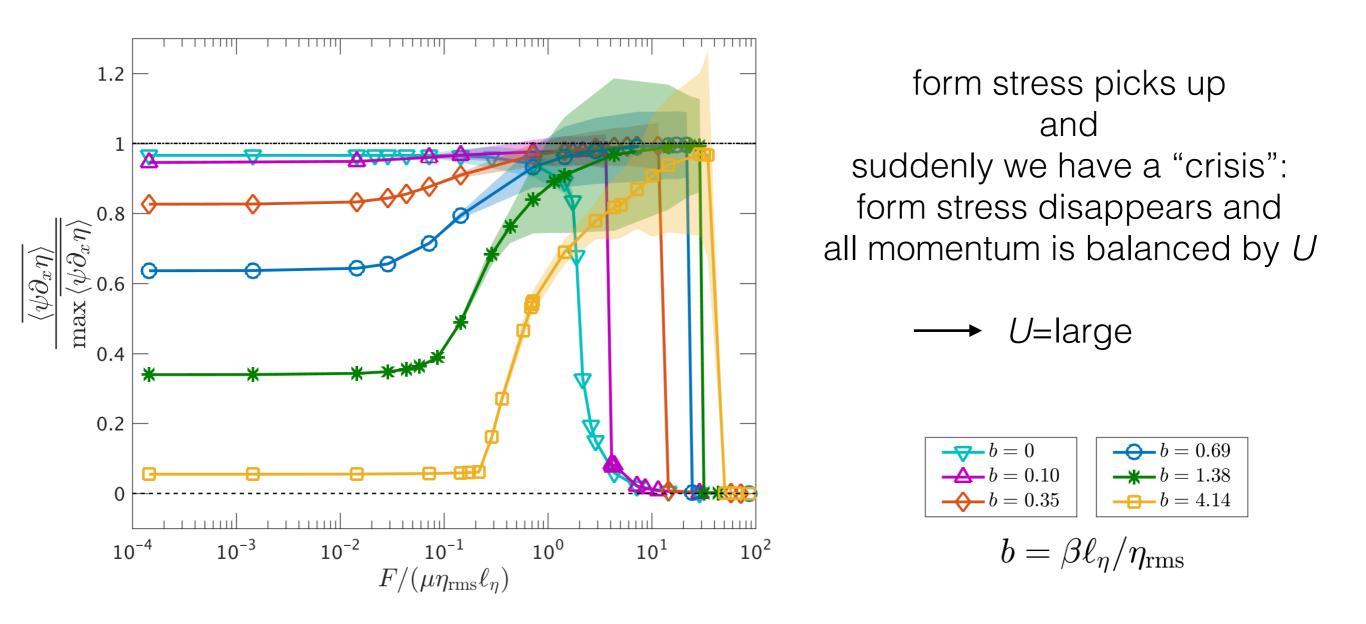
#### how does U respond to wind increase?



#### how does the form stress respond to wind increase?



#### how does the form stress respond to wind increase?



"crisis" occurs for all *b*>0

the regime 
$$\frac{F}{\mu\eta_{\rm rms}\ell_\eta}\ll 1$$
 &  $b=\beta\ell_\eta/\eta_{\rm rms}\gtrsim O(1)$ 

assuming a regular perturbation expansion for  $\psi$  and Uwe get that to first order

$$J(\psi - Uy, \eta + \beta y) = 0$$
$$F - \mu U - \langle \psi \partial_x \eta \rangle = 0$$

and using the eddy energy equation

$$U_0 = \frac{F/\mu}{1+1/b^2} \quad , \quad \langle \psi_0 \partial_x \eta \rangle = \frac{F}{1+b^2}$$

the regime 
$$\frac{F}{\mu\eta_{\rm rms}\ell_\eta}\ll 1$$
 &  $b=\beta\ell_\eta/\eta_{\rm rms}$ =0

it turns out that the problem is mathematically homomorphic to the steady state solution of the advection of a passive scalar by a flow in the presence of a large-scale concentration gradient

$$\mathsf{J}(\phi, c - Gy) = \kappa \nabla^2 c \qquad \qquad \mathsf{J}(\eta, \psi - Uy) = \mu \nabla^2 \psi$$

#### the analogy

$$\mathsf{J}(\phi, c - Gy) = \kappa \nabla^2 c$$

streamfunction concentration diffusion coefficient large-scale conc. gradient

$$Pe = \phi_{rms}/\kappa$$

$$\mathrm{Nu} = 1 + \frac{\langle c \partial_x \phi \rangle}{\kappa G}$$

for cellular flows and high Peclet numbers the concentration is confined to the places  $\phi=0$ 

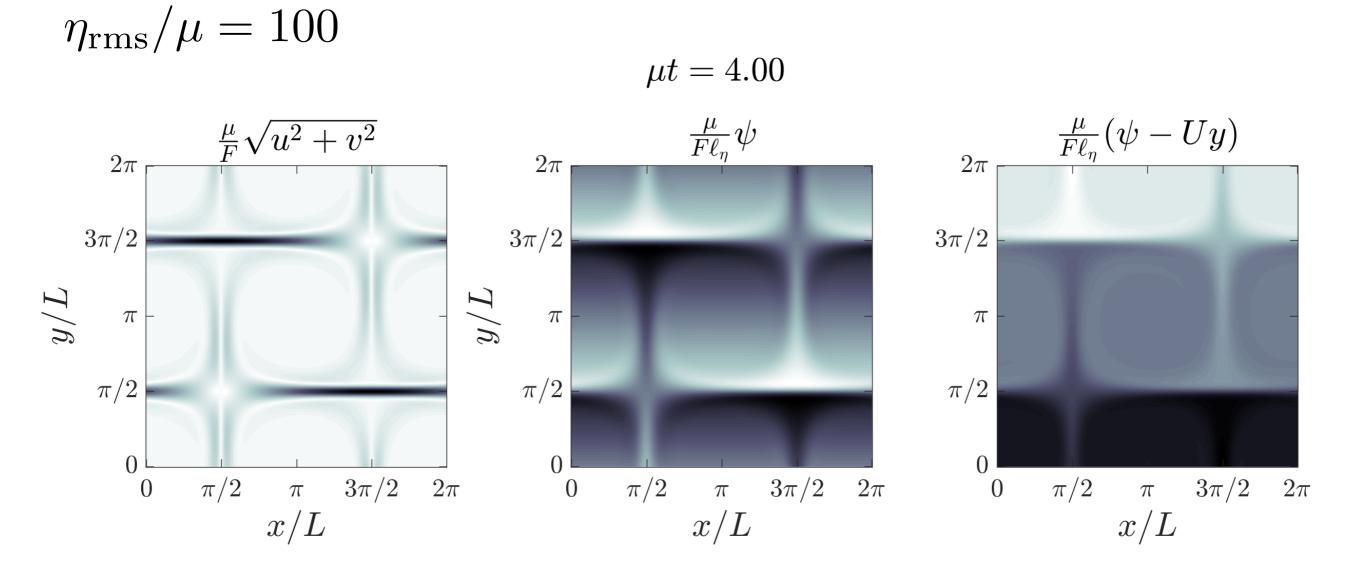
$$\mathsf{J}(\eta, \psi - Uy) = \mu \nabla^2 \psi$$

topography streamfunction dissipation coefficient large-scale flow

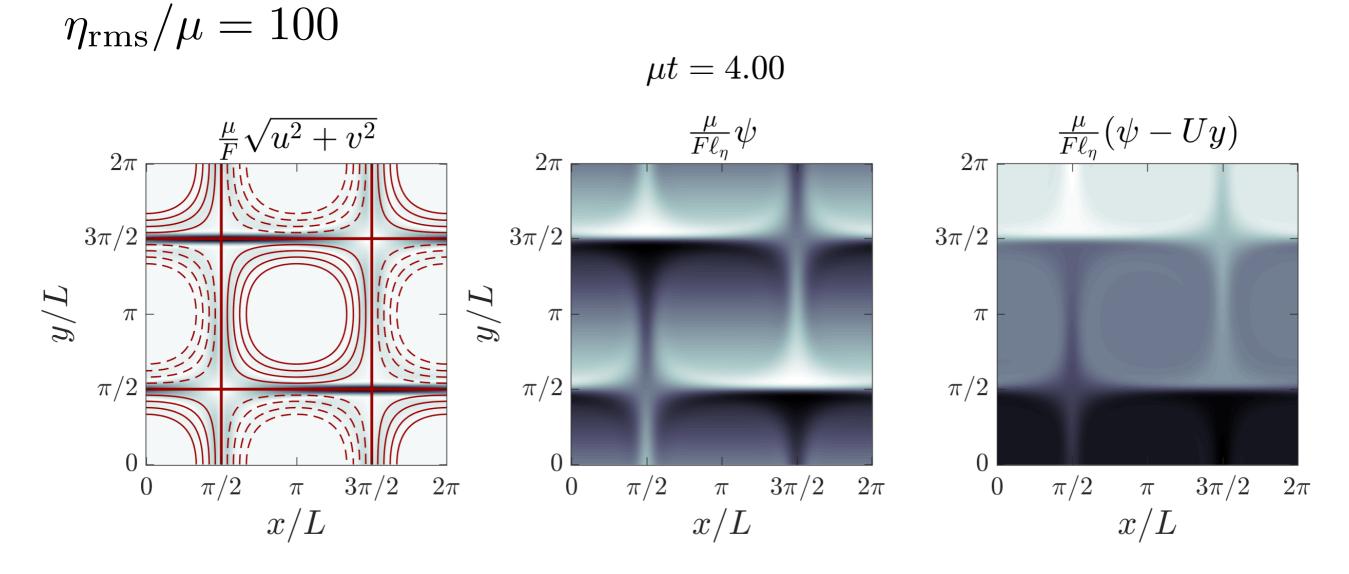
$$Pe_{\eta} = \eta_{rms}/\mu$$
$$Nu_{\eta} = 1 + \frac{\langle \psi \partial_x \eta \rangle}{\mu U}$$

?

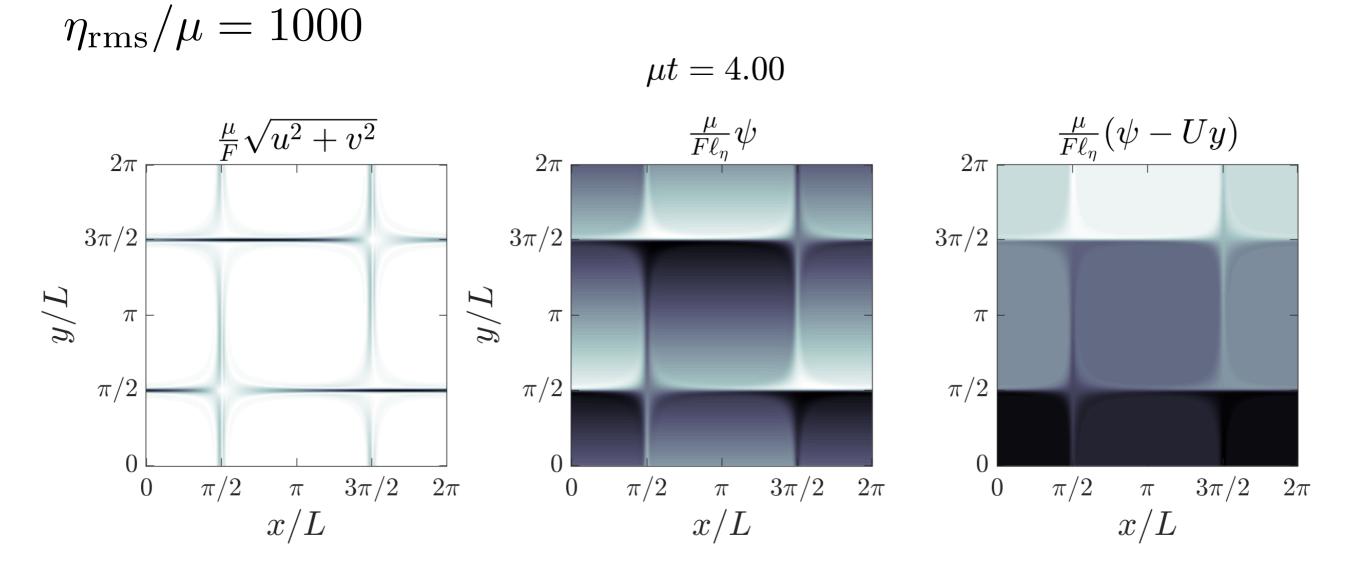
#### "cellular" topography



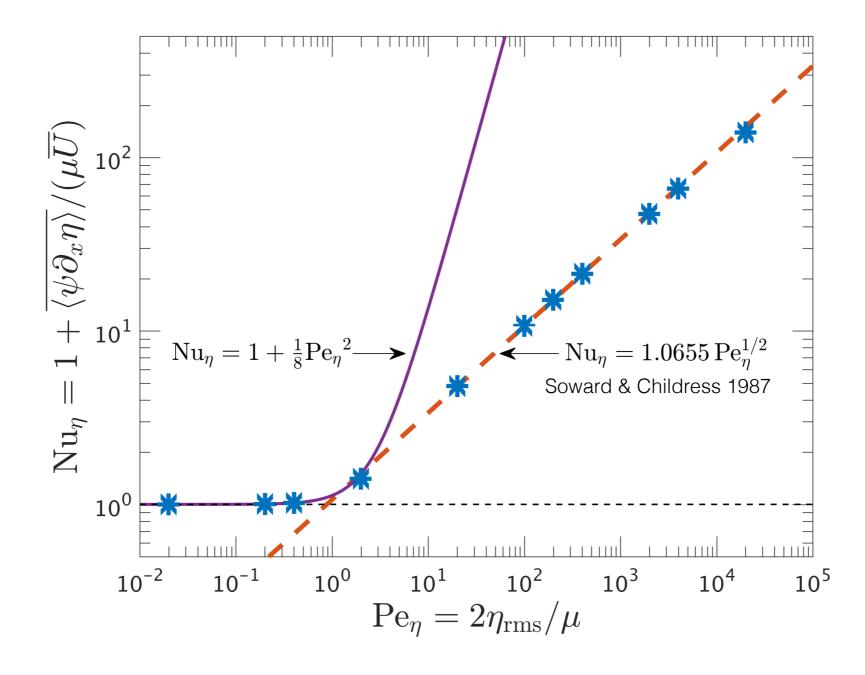
#### "cellular" topography



#### "cellular" topography



#### "Nusselt" scaling for "cellular" topography



$$\eta_{\rm rms}/\mu = 2$$

$$3\pi/4$$

$$3\pi/4$$

$$\int_{0}^{3\pi/4} \pi/2$$

$$\pi/4$$

$$\int_{0}^{\pi/4} \pi/4$$

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$$\pi/4$$

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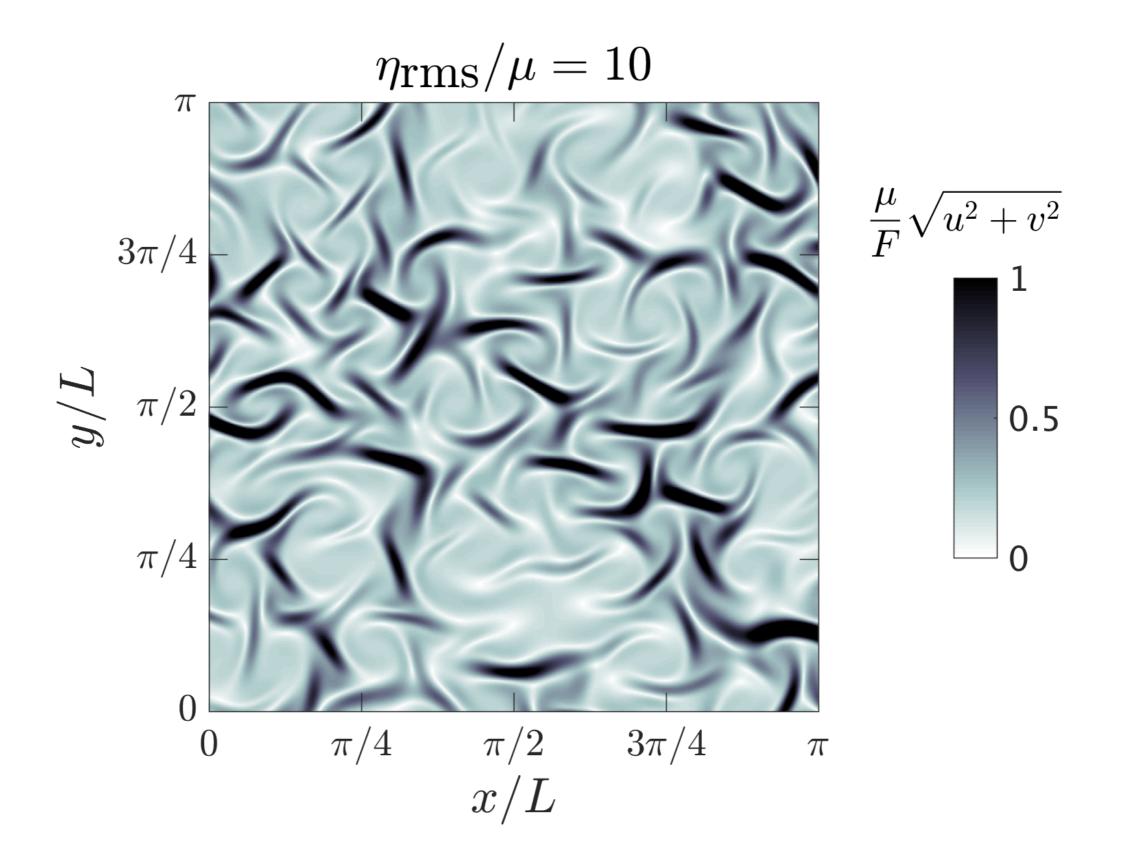
$$3\pi/4$$

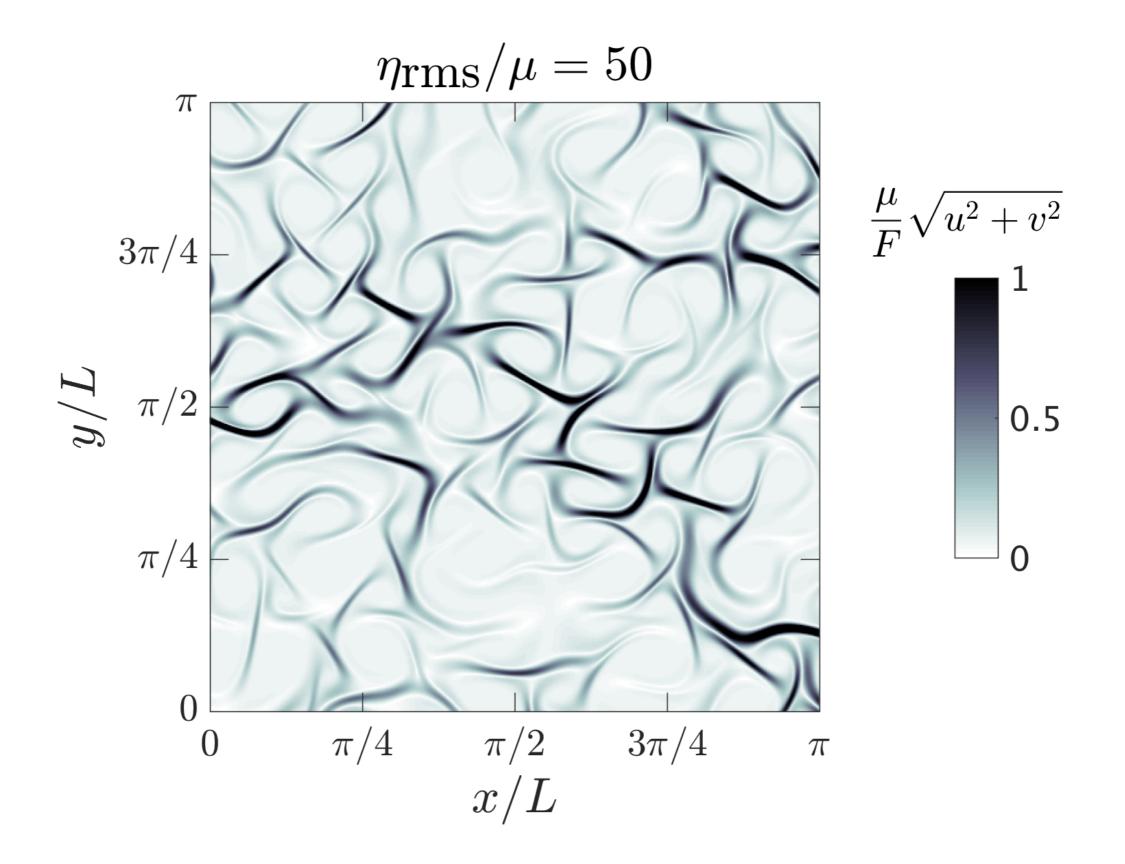
$$\pi/4$$

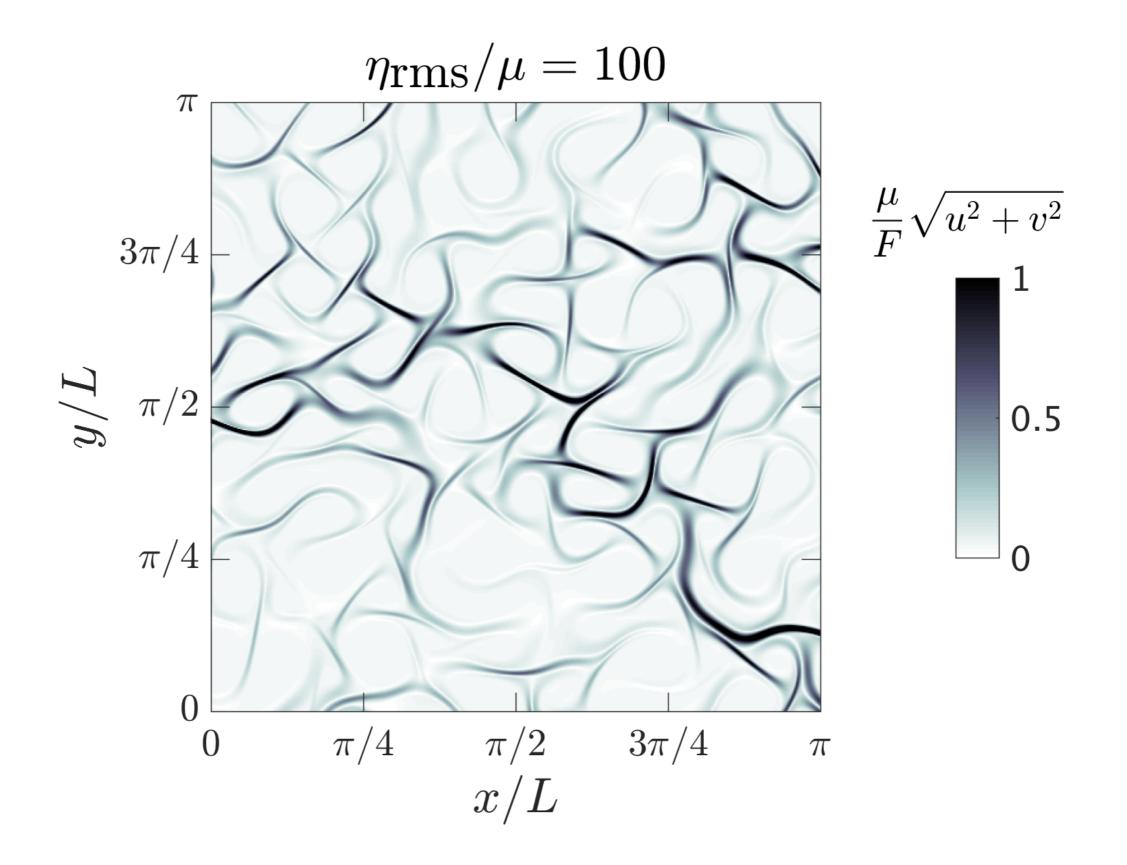
$$\pi/2$$

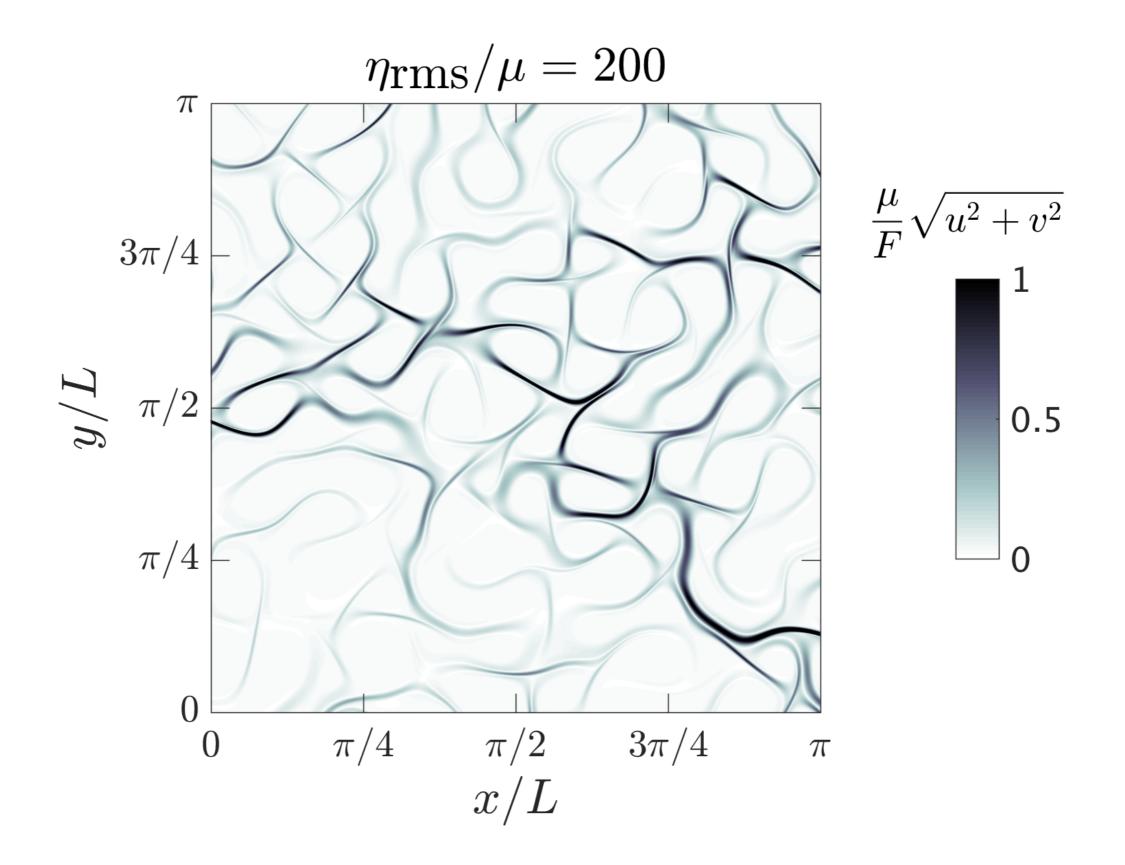
$$3\pi/4$$

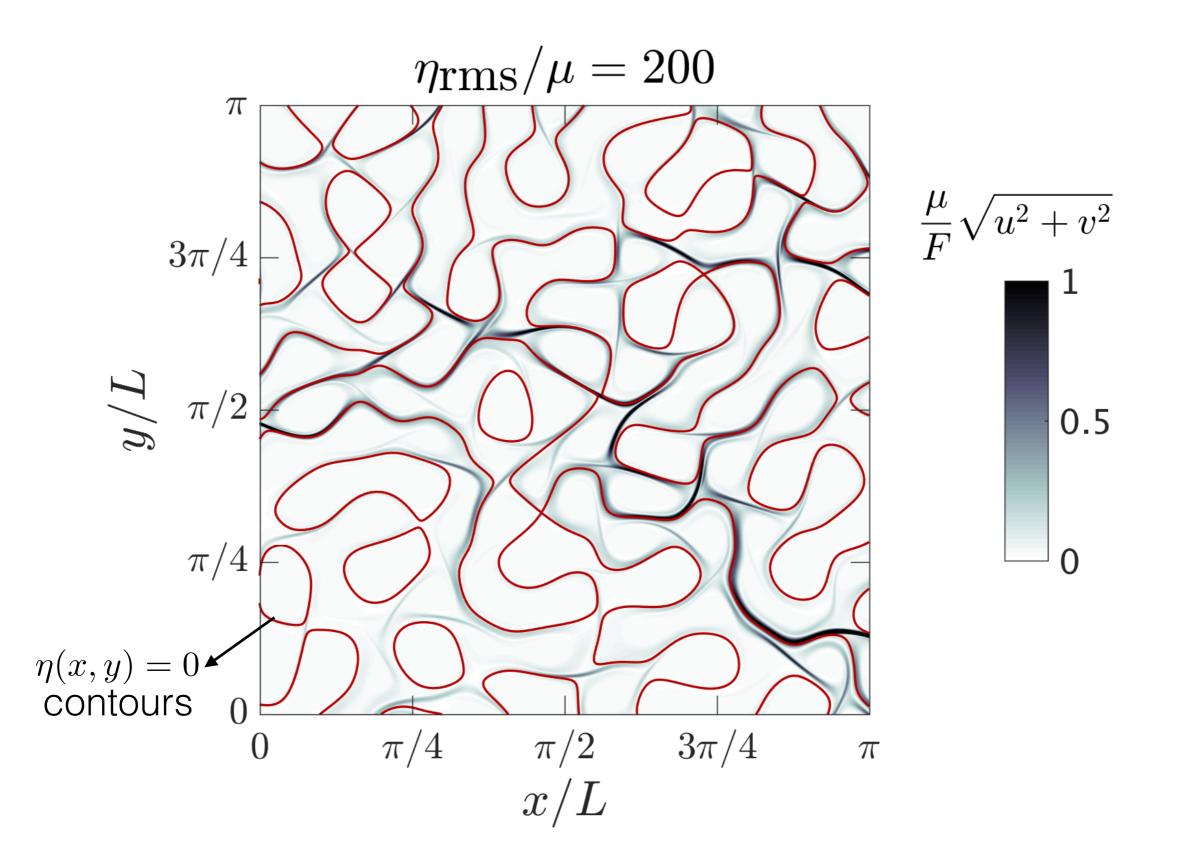
$$\pi/4$$

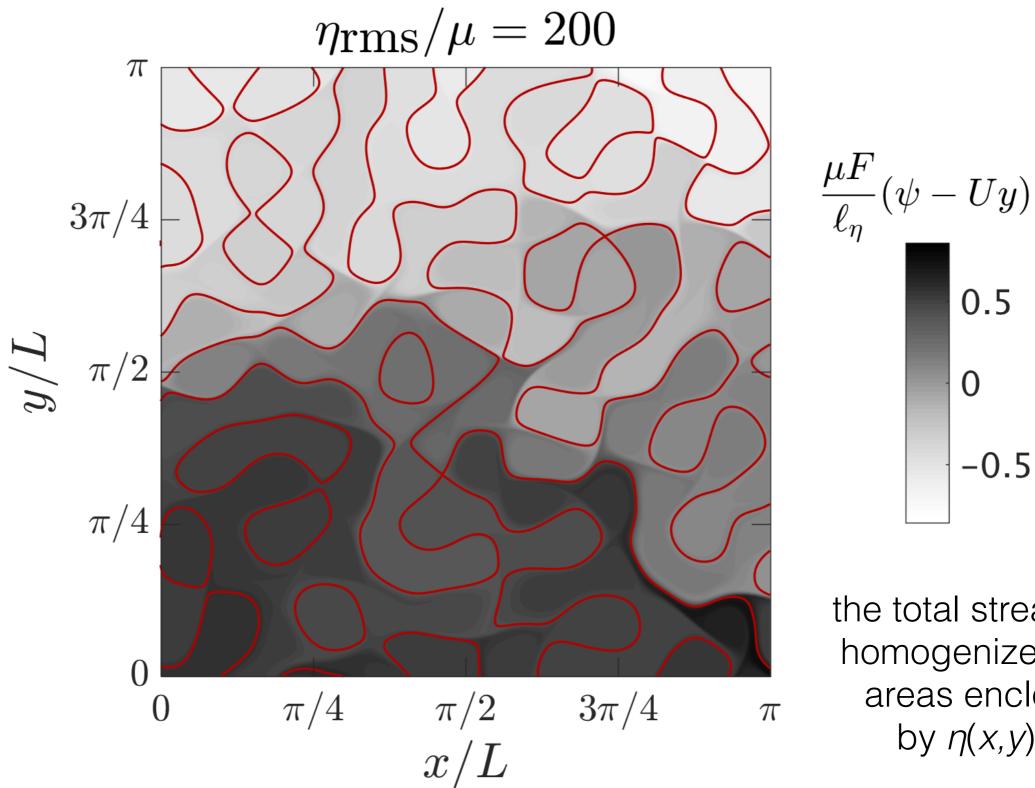












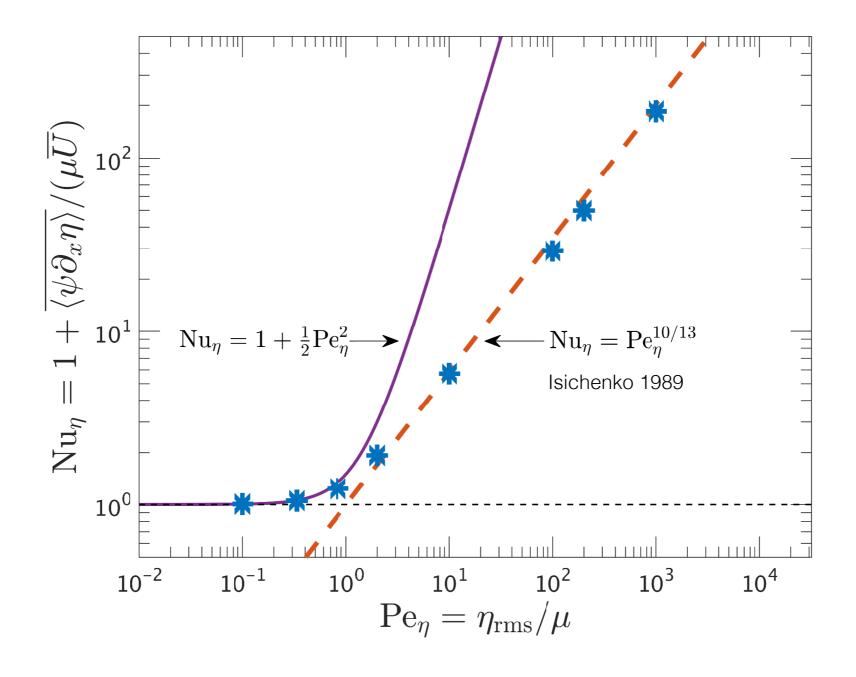
the total streamflow homogenizes over areas enclosed by  $\eta(x,y)=0$ 

-0.5

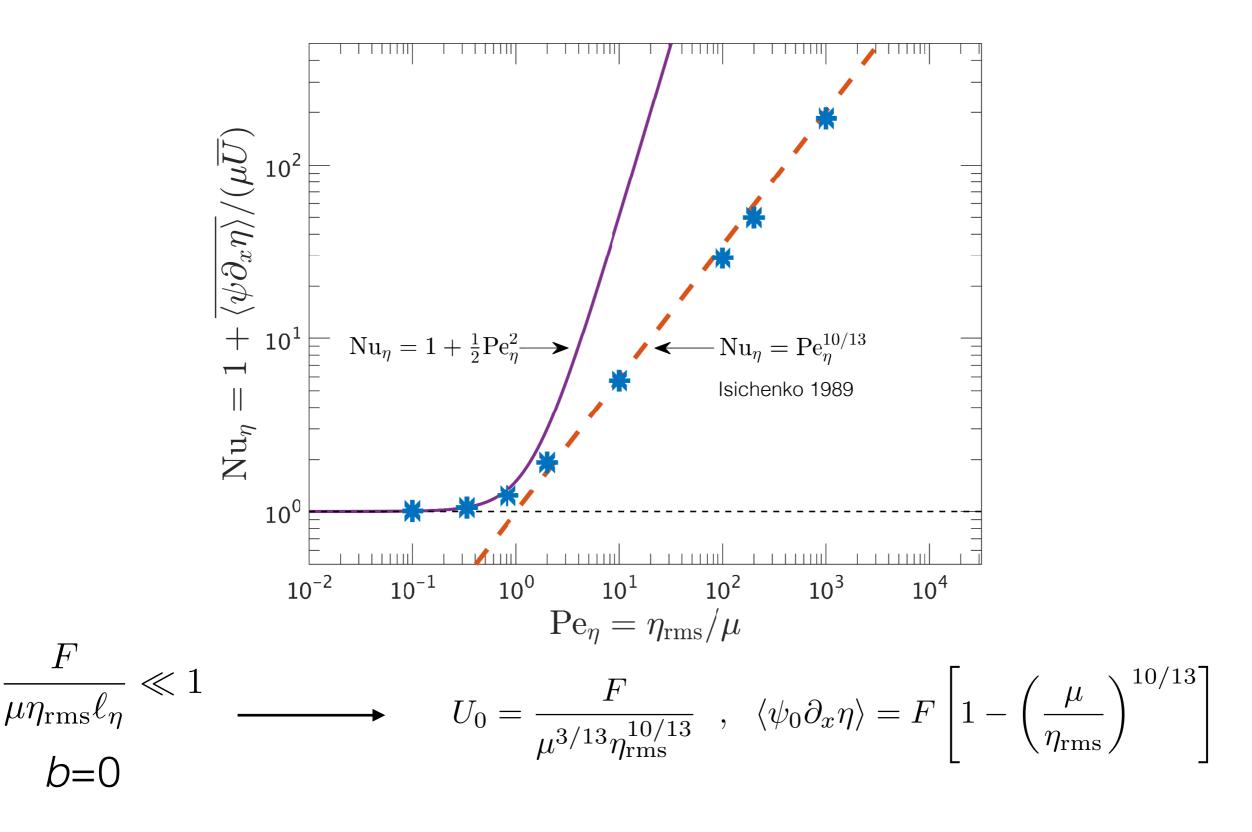
0.5

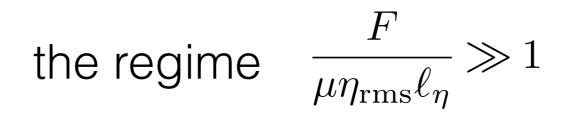
0

#### "Nusselt" scaling for random monoscale topography



## "Nusselt" scaling for random monoscale topography





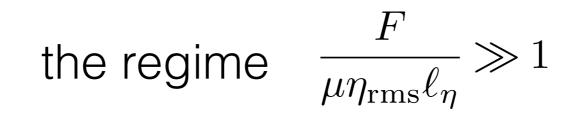
assuming a regular perturbation expansion for  $\psi$  and U we get to first order:

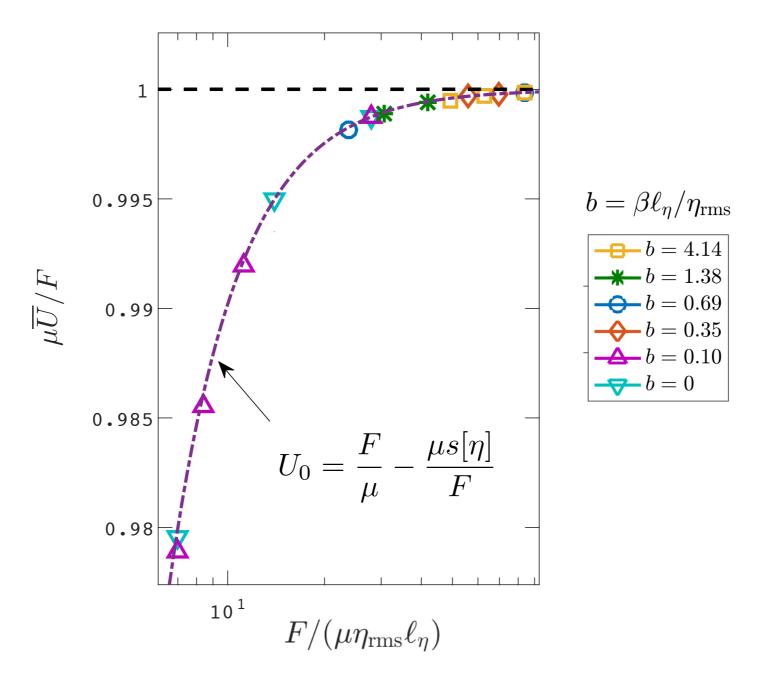
$$J(\psi - Uy, \eta + \beta y) = -\mu \nabla^2 \psi$$
$$F - \mu U - \langle \psi \partial_x \eta \rangle = 0$$

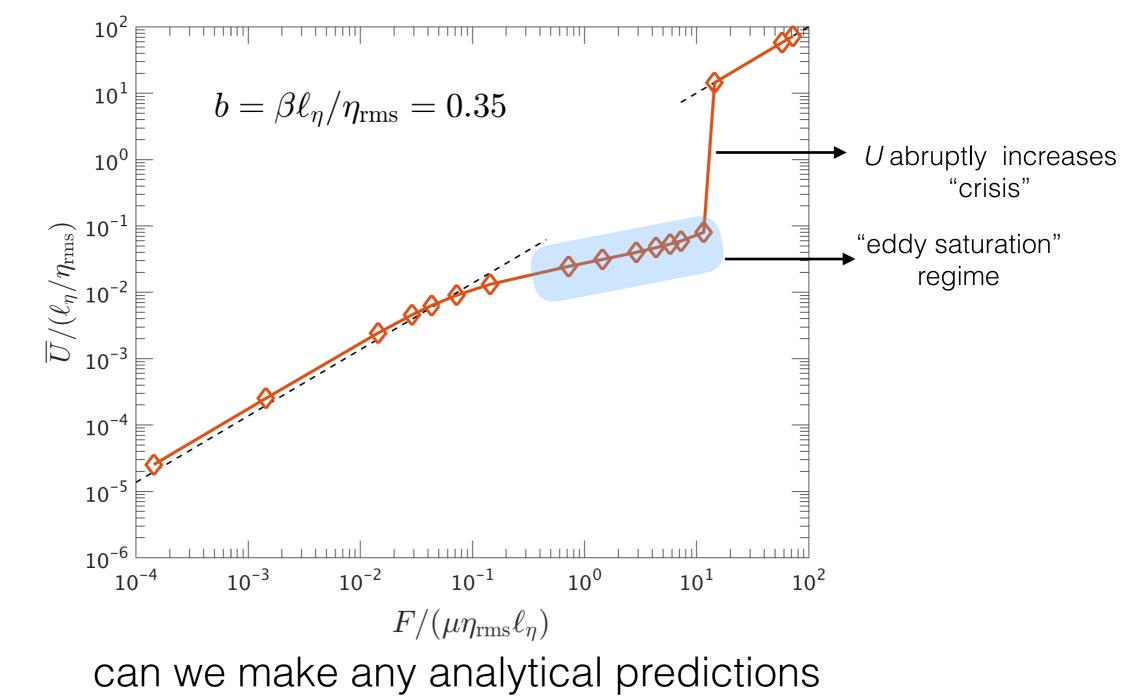
and using the eddy energy equation

$$U_0 = \frac{F}{\mu} - \frac{\mu s[\eta]}{F} \quad , \quad \langle \psi_0 \partial_x \eta \rangle = \frac{\mu^2 s[\eta]}{F} \qquad s[\eta] = \sum_{\mathbf{k}} \frac{|\hat{\eta}(\mathbf{k})|^2}{|\mathbf{k}|^2}$$

independent of b







regarding critical F and U at the eddy-saturation regime?

SSD?

#### Conclusions

- In regions with no continental boundaries topography/topographic form stress plays a crucial role in setting up the large-scale oceanic currents.
- We demonstrated that quasi-geostrophic theory, even with a simple 1-layer model, can capture the existence of an eddy-saturation regime.
- ▶ We derived a bound based on energy constraint for the form stress.
- We have seen that as the wind stress increases the momentum imparted by the ocean is balanced mostly by the form stress and only little by bottom drag... until a threshold wind value is reached ("crisis") when form stress breaks down and get very large U in order to get balance.
- Things are yet to be done; especially in understanding the regime prior to the "crisis".